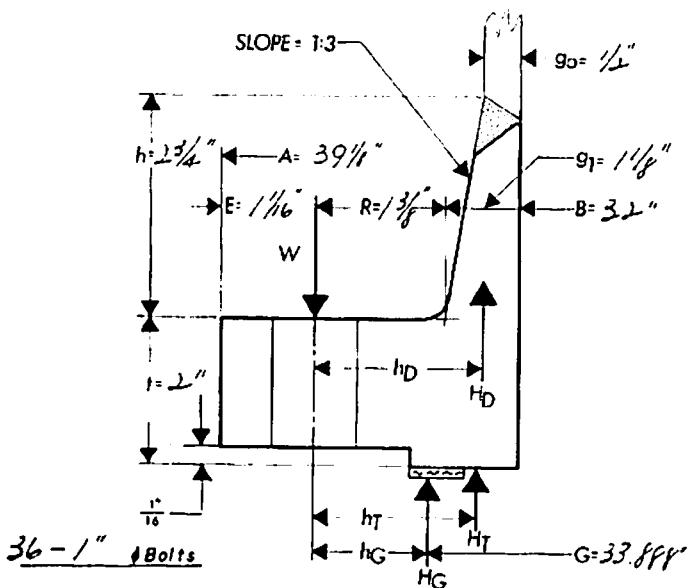


EXAMPLE 1

WELDING NECK FLANGE DESIGN

1 DESIGN CONDITIONS		2 GASKET	FACE	3 FROM Fig. UA-49
Design Pressure, P	400	33" ID X 36" OD X 1 1/16"	34 1/2" OD X 1 1/16" RF	$N = 0.750"$
Design Temperature	500°F	74°F ASB. COMP.		$b = 0.306"$
Flange Material	A105			$G = 33.888"$
Bolting Material	A 193-B7			$r = 3700$
Corrosion Allowance	0			$m = 2.750$
4 LOAD AND BOLT CALCULATIONS				
Allowable Stress	Flange	Design Temp., S_{f0} 17,500 Atm. Temp., S_{f0} 17,500	$W_{m2} = b\pi G_y = 120409$ $H_p = 2b\pi G_m P = 71713$	$A_n = \frac{\pi r^2}{4} W_{m2}/S_0$ or $W_{m1}/S_b = 17.299$ $A_b = 19.836$
	Bolting	Design Temp., S_b 25,000 Atm. Temp., S_b 25,000	$H = G^2 P/4 = 360771$ $W_a = H_p - H = 432484$	$W = .5(A_n + A_b)S_c = 464192$
CONDITION	LOAD	X	LEVER ARM	=
5 Operating	$H_D = \pi B^2 P/4 = 321699$ $H_G = W_a - H = 71713$ $H_T = H - H_D = 39072$		$h_D = R + S_g = 1.938"$ $h_G = .5(C - G) = 1.556"$ $h_T = .5(R + g + h_G) = 2.028"$	$M_D = H_D h_D = 623272$ $M_G = H_G h_G = 111599$ $M_T = H_T h_T = 79242$ $M_o = 814133$
Seating	$H_G = W = 464192$		$h_G = .5(C - G) = 1.556"$	$M_G = 722371$
8 Allowable Stress	STRESS CALCULATION—Operating			6 K AND HUB FACTORS
1.5 S_{f0}	Long. Hub, $S_H = f_m a / \lambda g_i^2 = 22865$			$K = A/B = 1.223$ $t = 1.130$ $Z = 5.041$ $Y = 9.773$ $U = 10.740$ $g_1/g_o = 2.250$ $h_o = \sqrt{8g_o} = 1.000$
S_{f0}	Radial Flg., $S_R = \beta m_a / \lambda t^2 = 10982$			$f = 0.777$ $v = 0.162$ $t = 1.000$ $d = \frac{U}{V} t_o g_o^2 = 66.49$
S_{f0}	Tang. Flg., $S_T = m_a Y / t^2 - Z S_R = 6800$			
S_{f0}	$\text{great } .5(S_H + S_R) \text{ or } .5(S_H + S_T) = 16923$			
9 Allowable Stress	STRESS CALCULATION—seating			7 STRESS FORMULA FACTORS
1.5 S_{f0}	Long. Hub, $S_H = f_m a / \lambda g_i^2 = 20288$			$I = 2.000$ $\alpha = t_o + 1 = 1.348$ $\beta = 4/3 t_o + 1 = 1.518$ $\gamma = a/t = 0.759$ $\delta = t^2/d = 0.120$ $\lambda = \gamma + \delta = 0.879$ $m_o = M_o/B = \text{operating } 2544.2$ $m_o = M_o/B = \text{seating } 2257.4$
S_{f0}	Radial Flg., $S_R = \beta m_a / \lambda t^2 = 9744$			
S_{f0}	Tang. Flg., $S_T = m_a Y / t^2 - Z S_R = 6033$			
S_{f0}	$\text{great } .5(S_H + S_R) \text{ or } .5(S_H + S_T) = 15016$			



G+W Taylor-Bonney Division



Computed DLS Date 7-17-79

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